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Author(s):	Kulesza, Joel A. Martz, Roger Lee
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Evaluation of the Pool Critical Assembly Benchmark with Explicitly Modeled Geometry using MCNP6's Unstructured Mesh Capabilities

Joel A. Kulesza^{1,2} and Roger L. Martz²

¹University of Michigan, Department of Nuclear Engineering & Radiological Sciences 2355 Bonisteel Blvd., Ann Arbor, MI, 48109
²Los Alamos National Laboratory, Monte Carlo Methods, Codes, and Applications Group P.O. Box 1663, Los Alamos, NM, 87545

jkulesza@umich.edu, martz@lanl.gov

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Outline

Introduction & Background

Experimental and Analytical Model

Calculational Process

Results & Summary



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Objective: introduce reactor dosimetry community to MCNP6's unstructured mesh (UM) capabilities with a familiar benchmark problem

- Oak Ridge National Laboratory Pool Critical Assembly
 - Originally published in 1997 by Remic and Kam (1997)
 - Recently analyzed in MCNP (using CSG) by Kulesza and Martz (2017)
- First time analyzing PCA with Monte Carlo on UM
 - It is hoped that this work will stimulate interest among the reactor dosimetry community for incorporating UM into their own analyses
- This work expands the set of MCNP6 UM validation analyses

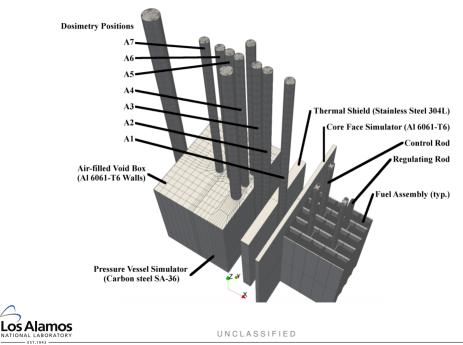


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Geometry Overview



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Unstructured Mesh Modeling Process

- UM considerations
 - 1. Accurate representation of geometry
 - 2. Sufficient granularity for results visualization
 - 3. Well-behaved elements
- Mesh creation process summary
 - 1. Create model geometry in SpaceClaim
 - 2. Export SpaceClaim model to STEP format
 - 3. Import STEP into Abaqus
 - 4. Define element sets and materials within Abaqus
 - 5. Define mesh seed spacing for each part in Abaqus
 - 6. Create mesh in Abaqus
 - 7. Combine meshed parts into assembly
 - 8. Write input for MCNP6
 - Steps 3–7 automated via Python within Abaqus
 - Some tuning necessary for Steps 5 & 6

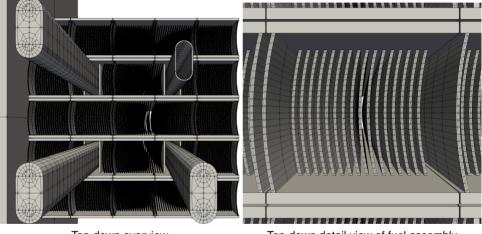


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PCA Core Geometry



Top-down overview

Top-down detail view of fuel assembly



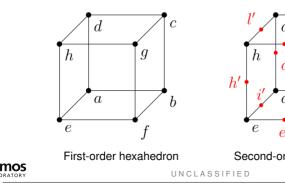
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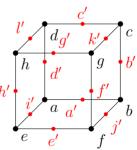
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Unstructured Mesh Statistics

- 932 SpaceClaim parts
 - Each fuel plate is two parts: fuel & cladding
 - The RPV is split into 3 parts to ease meshing: 935 total
- 745,248 first-order hexahedral elements total
 - No part with more than 12,000 elements
 - Fuel has ~450 elements
 - Fuel clad has ~1,300 elements
 - Mesh generation requires ~10 minutes





Second-order hexahedron

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Step 1: Criticality Calculation for Source Term

- Remic and Kam (1997) provide shape functions to define source
- This work calculates the fission source directly
 - Perform an eigenvalue calculation to determine source points
 - Convert source points into a fixed surface source
- Benefits of this approach
 - A near-critical eigenvalue helps validate the model
 - "Easier" to define in a Monte Carlo analysis
- Results of this approach
 - Eigenvalue usually within 50 pcm of unity
 - Eigenvalue 1σ uncertainty of ~50 pcm
 - Mesh tallies and UM edits can confirm source term behavior

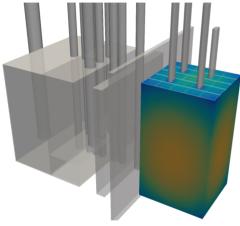


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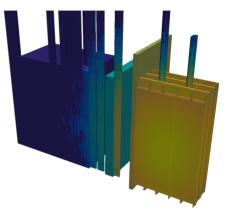
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Visual Validation of Source Term



Core-wide meshtally



UM-wide track-length edits

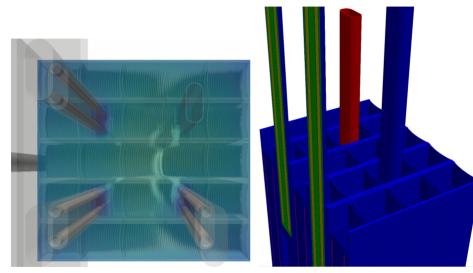


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Confirmatory Views of Source Term & Geometry



Top-down view of core with transparent geometry

Geometry colored by material



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Step 2: Conversion of Fission Sites to Fixed Source

- Uses MCNP6's surface source read/write (SSR/W) capabilities
 - ► In this special case, SSR/W processes fission sites, not surfaces
- Process summary
 - 1. Set neutrons/batch and number of batches
 - Product gives number of source points processed
 - Can lead to source particle weight adjustments
 - 2. Define the cells that contain fission sites
 - 3. MCNP6 will read the srctp file and produce a surface source (wssa) file
- Process tutorial available in MCNP Criticality Calculations Course¹
 - Problem P-16, Criticality Accident Alarm System Calculations

¹ https://laws.lanl.gov/vhosts/mcnp.lanl.gov/classes/classinformation.shtml



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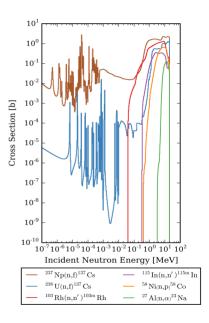
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Step 3: Final Fixed Source Calculations

- Reuse ADVANTG-produced weight windows from Kulesza and Martz (2017)
 - One set of weight windows per reactions
 - Constructed based on IRDFF v.1.05 dosimetry responses
- 180 total calculations, 512 processors each
 - ► 30 independent 1-million history runs × 6 reactions
 - Total computer time: 554.5 hours (283,892 core hours)



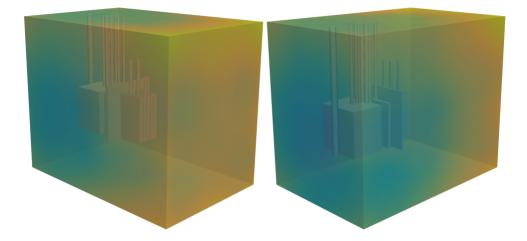


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Reasonable Weight Window Behavior



• Problem domain: $-150 \le x \le 150, -100 \le y \le 100, -100 \le z \le 150$

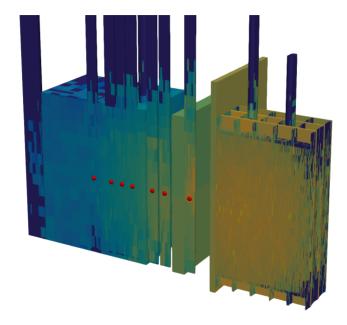


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Unstructured Mesh Flux Edit — $^{27}Al(n,\alpha)$ Execution





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Calculation / Experiment (Remic and Kam, 1997) Ratios

Loc.	²⁷ Al(n, α)	⁵⁸ Ni(n,p)	¹⁰³ Rh(n,n')	¹¹⁵ ln(n,n')	²³⁸ U(n,f)	²³⁷ Np(n,f)	Avg.
A1	0.91	1.00	1.11	1.04	_	1.08	1.03
A2	0.99	1.09	—	1.03	—		1.04
A3	1.04	1.11	—	1.14	—	1.27	1.14
A4	1.29	1.11	1.09	1.06	1.04	1.11	1.12
A5	1.15	1.12	1.04	1.10	0.97	1.08	1.08
A6	_	1.18	1.06	1.06	1.01	1.10	1.08
A7	_	—	_	—	—	1.30	1.30
Avg.	1.08	1.10	1.08	1.07	1.01	1.16	1.09

²⁷Al values have higher-than-desired statistical uncertainties

- ²³⁷Np values have been observed to disagree historically
- Average agreement (by reaction, position, and overall) still reasonable



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Calculation / Experiment (Fero et al., 2001) Ratios

Loc.	²⁷ Al(n, α)	⁵⁸ Ni(n,p)	¹⁰³ Rh(n,n')	¹¹⁵ ln(n,n')	²³⁸ U(n,f)	²³⁷ Np(n,f)	Avg.
A1	0.92	1.01	1.11	1.05	—		1.02
A2	1.00	1.09	1.15	1.04	—		1.07
A3	1.05	1.12	1.17	1.16	1.19	1.24	1.16
A4	1.30	1.13	1.09	1.06	1.08	1.13	1.13
A5	1.13	1.14	1.02	1.10	1.03	1.12	1.09
A6	—	1.20	1.02	1.05	1.06	1.12	1.09
A7	_	—	1.05	1.09	1.04	1.29	1.12
Avg.	1.08	1.12	1.09	1.08	1.08	1.18	1.10

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Summary & Future Work

- Demonstrated MCNP6 UM ability to perform reactor dosimetry analyses
 - Situation-specific source generation & analysis workflow
 - Techniques for validation
 - Flexibility in geometry & results visualization
- Extended MCNP6 UM validation (overall C/E ~1.10)
 - More work is needed to reduce statistical uncertainties
 - Especially true of ²⁷Al(n,α)
 - Value in introducing track-length tallies to verify point detectors
- Short-term future work
 - Need to investigate why calculation-to-experiment ratios >1
- Longer-term future work
 - More effective workflow to generate weight windows
 - Should weight windows be generated on the UM? How?



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Contact Information

Joel A. Kulesza Mobile: +1 (734) 223–7312 Email: jkulesza@umich.edu

Roger L. Martz Office: +1 (505) 664–0900 Email: martz@lanl.gov



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