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Author(s):	Carney, Sean E. Brown, Forrest B. Kiedrowski, Brian C. Martin, William R.
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Higher-Mode Applications of Fission Matrix Capability for MCNP

Sean Carney, Forrest Brown, Brian Kiedrowski, William Martin

Monte Carlo Codes Group, LANL NERS Dept., University of Michigan



U.S. Department of Energy









Introduction

- Motivation
- Preliminary theory
- Past findings
- Eigenmode expansion
- Forward Flux Modes
- Fission Kernel Deflation
- Adjoint Flux Weighting
- Conclusions, Future Work

Carney, Brown, Kiedrowski, Martin, "Fission Matrix Capability for MCNP Monte Carlo", TANS 107, San Diego, 2012 Brown, Carney, Kiedrowski, Martin, "Fission Matrix Capability for MCNP, Part I - Theory", M&C-2013, 2013 Carney, Brown, Kiedrowski, Martin, "Fission Matrix Capability for MCNP, Part II - Applications", M&C-2013, 2013



- Problem: Direct & precise calculation of small changes from finetuning design with Monte Carlo is time-consuming:
 - computationally (precise deltas from stochastic results)
 - man-power (search of design space)
- Perturbation theory: search design space more efficiently, condense design calculations
- 2nd order perturbation theory: extend applicability in design space
 - Forward problems
 - Burnup
 - Control rod movement/interaction
 - BWR/Xenon power oscillations
 - Inverse problems
 - Detector response-guided calculations
 - Requires higher-mode flux information--both forward and adjoint
- Additionally: further insight into power iteration with higher modes



Preliminary Theory





Start with the k-eigenvalue form of the transport equation

$$\mathbf{M} \cdot \Psi_n(\vec{r}, E, \hat{\Omega}) = \frac{1}{K_n} \frac{\chi(\vec{r}, E)}{4\pi} S_n(\vec{r})$$

Infinite number of solutions: most recognized & physical is fundamental (*n=0*)

$$\mathbf{M} \cdot \Psi_n(\vec{r}, E, \hat{\Omega}) = \hat{\Omega} \cdot \nabla \Psi_n(\vec{r}, E, \hat{\Omega}) + \Sigma_T(\vec{r}, E) \Psi_n(\vec{r}, E, \hat{\Omega}) \\ - \iint dE' d\hat{\Omega}' \Sigma_S(\vec{r}, E' \to E, \hat{\Omega}' \to \hat{\Omega}) \Psi_n(\vec{r}, E', \hat{\Omega}')$$

Net loss operator

$$S_n(\vec{r}) = \iint dE' d\hat{\Omega}' \nu \Sigma_F(\vec{r}, E') \Psi_n(\vec{r}, E', \hat{\Omega}')$$

Theory



- Using,
 - Green's function
 - Integral transport equation
 - Discretization of space into N mesh cells

Eigenvalue problem (without approximation):

$$S_{n,I} = \frac{1}{K_n} \sum_{J=1}^N F_{I,J} S_{n,J}$$

 $F_{I,J}$ = next-generation fission neutrons produced in region I, for each average fission neutron starting in region J (J \rightarrow I)

Discrete fission source

$$S_{n,I} = \int_{\vec{r} \in V_I} d\vec{r} \, S_n(\vec{r})$$

Fission matrix element $F_{I,J} = \int_{\vec{r} \in V_I} d\vec{r} \int_{\vec{r}_0 \in V_J} d\vec{r}_0 \ F(\vec{r}_0 \to \vec{r}) \frac{S_0(\vec{r}_0)}{S_{0,J}}$

Energy & angleintegrated Green's $F(\vec{r}_0 \rightarrow \vec{r}) = \iiint dE d\hat{\Omega} dE_0 d\hat{\Omega}_0 \nu \Sigma_F(\vec{r}, E) G(\vec{r}_0, E_0, \hat{\Omega}_0 \rightarrow \vec{r}, E, \hat{\Omega}) \frac{\chi(\vec{r}_0, E_0)}{4\pi}$ function, "fission kernel"



• In the equation for F,

- $S(r_0)/S_J$ is a local weighting function within region J--unknown if unconverged
- As $V_J \rightarrow 0$:
 - Discretization errors $\rightarrow 0$
 - Can accumulate tallies of F_{I,J} even if not converged
 - Left eigenvectors correspond to adjoint fission source modes:

$$S_n^{\dagger}(\vec{r}) = \int \int dE' d\hat{\Omega}' \frac{\chi(\vec{r}, E')}{4\pi} \Psi_n^{\dagger}(\vec{r}, E', \hat{\Omega}')$$

• Higher-order modes require finer mesh for convergence (mode -0 local weighting function deviates from higher modes)



Past Findings



- F_{I,J} tallies:
 - Previous F-matrix work: tally during neutron random walks
 - Present F-matrix work:

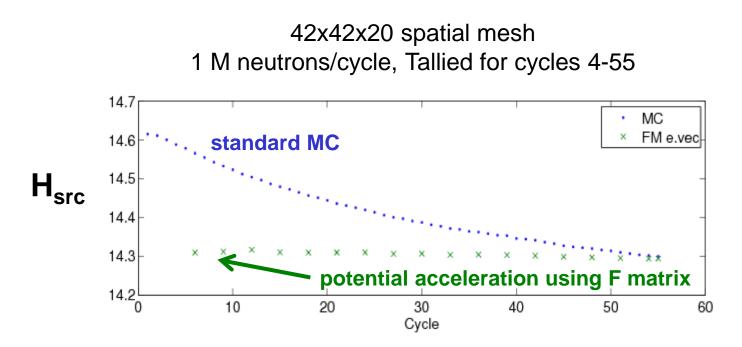
tally only point-to-point, using fission-bank in master proc (~free)

- Accumulate tallies over all cycles
 - skip first ~2 to reduce discretization error
- Sparse storage—coupling between mesh cells is localized
 - Compressed row storage
 - Very fine mesh—initially allocate some max number of elements
- Solve eigenvalue problem
 - Aggregate elements during post-processing
 - Sparse-solvers: Hotelling Deflation (this work), Arnoldi (much faster)



- Fission matrix can be used to accelerate convergence of the MCNP neutron source distribution during inactive cycles
- Duplicate/remove sites in fission bank to match F matrix fund. mode
- Impressive convergence improvement

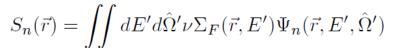
Kord Smith Challenge (3D Whole-Core)

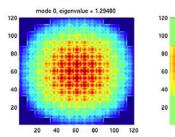


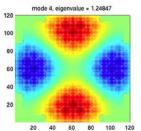
PWR – Eigenmodes for 120x120x1 Spatial Mesh

mode 2, eigenvalue = 1.27664

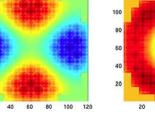


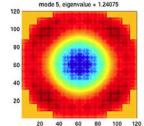






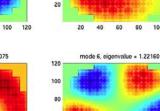
mode 8, eigenvalue = 1.19745

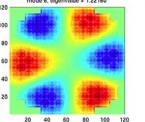


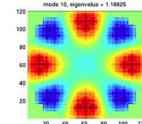


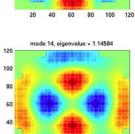
mode 9, eigenvalue = 1.19743

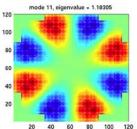
mode 1, eigenvalue = 1.27657





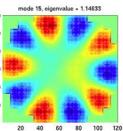






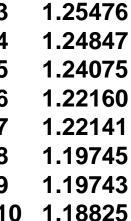
mode 3, eigenvalue = 1.25476

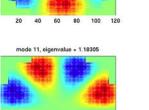
mode 7, eigenvalue = 1.22141



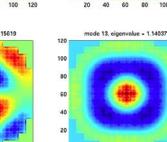
n	K _n				
0	1.29480				
1	1.27664				
2	1.27657				
3	1.25476				
4	1.24847				
5	1.24075				
6	1.22160				
7	1.22141				
8	1.19745				
9	1.19743				
10	1.18825				
11	1.18305				
12	1.15619				
13	1 14633				

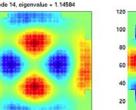
1.14633 1.14617 15 1.14584





mode 12, eigenvalue = 1.15619







Eigenmode Expansion



- Source convergence in Monte Carlo criticality calculations involves "powering out" the higher modes excited from the initial distribution
- Using pre-calculated forward/adjoint source modes, and biorthogonality, the cycle-by-cycle contributions of these modes can be estimated

Expansion of cycle-*c* source into \widehat{N} modes

$$F^c(\vec{r}) = \sum_{n=0}^{\hat{N}} a_n^c S_n(\vec{r})$$

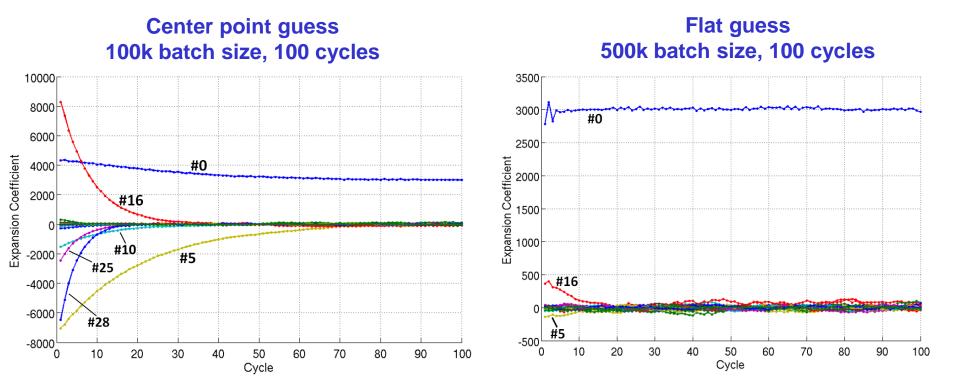
Magnitude of the expansion coefficients (found using inter-cycle fission sites)

$$a_n^c = \frac{\langle F^c(\vec{r}) S_n^\dagger(\vec{r}) \rangle}{\langle S_n(\vec{r}) S_n^\dagger(\vec{r}) \rangle}$$

- Three initial guesses ran for 2D PWR problem:
 - center point
 - corner point
 - flat distribution
- Source modes calculated with: 300 cycles, 500k batch size, 50x50x1 mesh

Center-Point & Flat Guesses

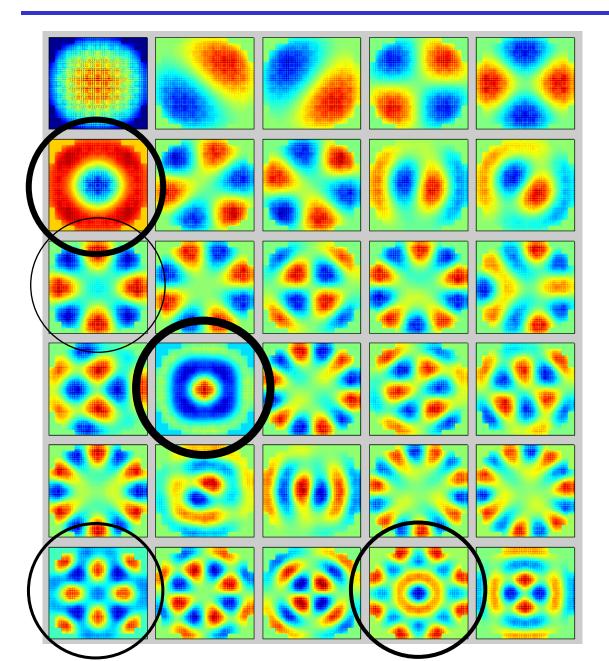


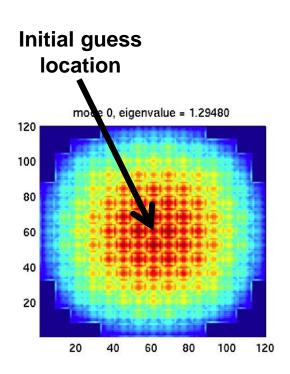


Radially-symmetric modes excited in both cases—more so for center-point

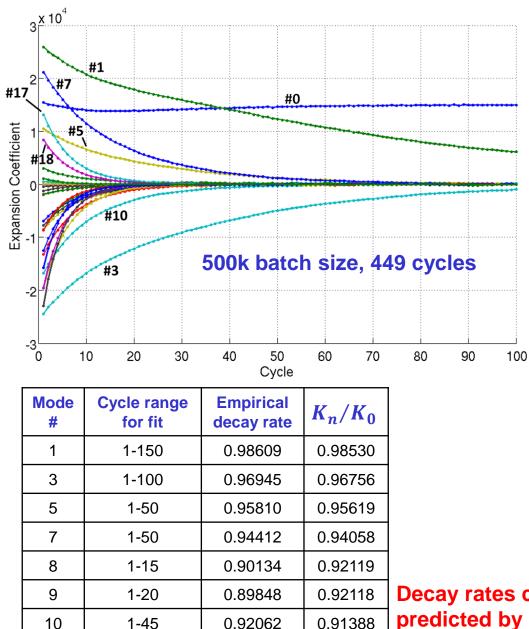
PWR – First 30 Eigenmodes

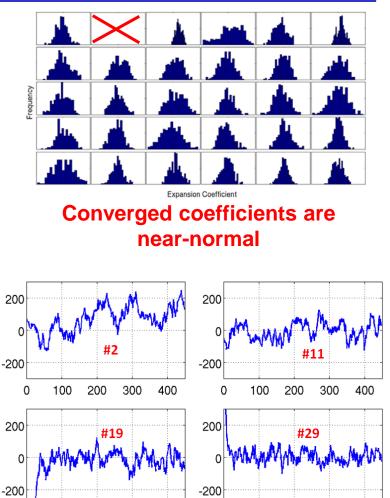






Corner-Point Guess





Lag-correlation of modes is a function of K_n/K_0

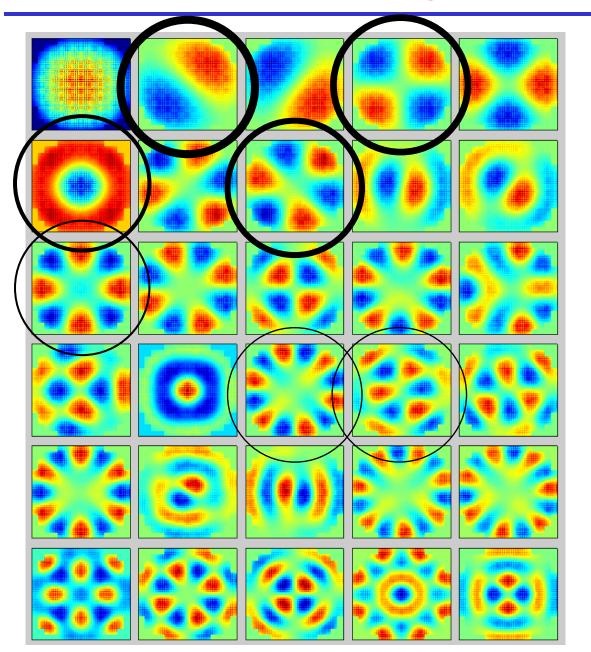
Decay rates can be predicted by eigenvalue

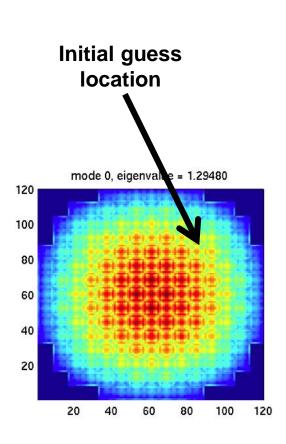
MCNP

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PWR – First 30 Eigenmodes









Forward Flux Modes



• Forward flux modes are calculated by running fixed source calculations on forward fission source modes

$$\Psi_n(\vec{r}, E, \hat{\Omega}) = \frac{1}{K_n} \mathbf{M}^{-1} \cdot \frac{\chi(\vec{r}, E)}{4\pi} S_n(\vec{r}) \qquad \mathbf{n} = \mathbf{0}, \mathbf{1}, \dots, \widehat{\mathbf{N}}$$

- Source is sampled in an analog manner
 - Alias table used for efficiency
 - Point within mesh cell is resampled until within fissionable material
 - Flag is added for sign of particle weight
 - Fission is treated as absorption (NONU card)
- Track-length flux mesh tally module FMESH used
- Possible efficiency gain: Sample source uniformly, keep vector of weights for different mode values

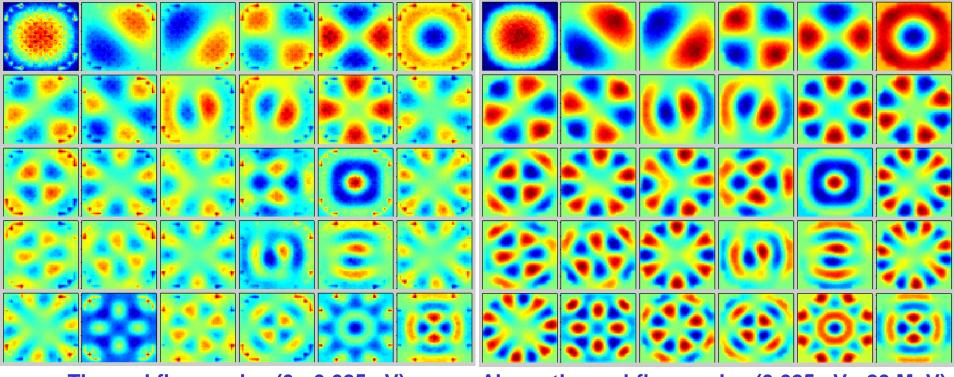


Source modes acquired with matrix tallied for 500 cycles, 500k batch size

Fixed source calculations performed with 500k histories

50x50x1 mesh

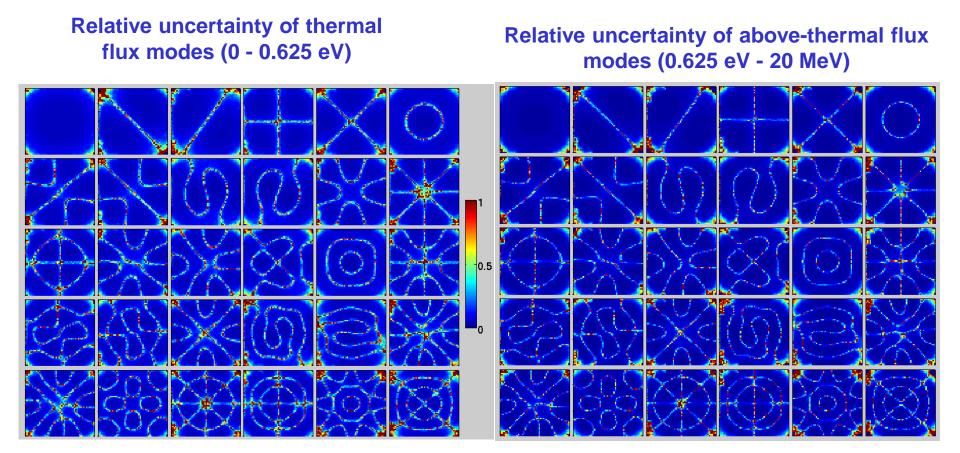
$$\int_{\vec{r} \in V_i} d\vec{r} \int_{E_g}^{E_{g-1}} dE \int_{4\pi} d\hat{\Omega} \, \Psi_n(\vec{r}, E, \hat{\Omega})$$



Thermal flux modes (0 - 0.625 eV)

Above-thermal flux modes (0.625 eV - 20 MeV)

Relative Uncertainty of Forward Flux Modes for 2D PWR problem



High relative uncertainties are strongly localized to inflection lines

men

8-20-2013



Fission Kernel Deflation



- Desired applications of modal information:
 - 2nd order perturbation theory (capture effect of flux pert. on eigenvalue)
 - Quasi-static calculations (model BWR instabilities, Xenon oscillations)
- These methods require weighting with higher-mode adjoint fluxes
- Continuous-energy Monte Carlo adjoint transport is intractable
- Mode-0 adjoint-weighted tallies are performed in MCNP using iterated fission probability (weigh by size of long-time fission chain):
 - In original generation, tallies are associated with a progenitor neutron
 - After L latent generations, the progeny of progenitors are followed for enough cycles to reach their asymptotic distribution (the fundamental mode)
 - In asymptotic generation, the progeny population is used for weighting of original tallies

 $\Psi^{\dagger}(\vec{r}_0, E_0, \hat{\Omega}_0) \alpha \langle F(\vec{r}' \to \vec{r})^L \cdot \iint dE' d\hat{\Omega}' G(\vec{r}_0, E_0, \hat{\Omega}_0 \to \vec{r}', E', \hat{\Omega}') \nu \Sigma_F(\vec{r}', E') \rangle_{\vec{r}}$

• Aside: With higher modes, the number of necessary latent generations can be quantified (as a function of space)



• Standard matrix deflation eliminates the effect of eigenvectors

$$F_{n} = F - \sum_{n'=0}^{n-1} K_{n'} \frac{S_{n'} S_{n'}^{\dagger}}{\langle S_{n'}^{\dagger} S_{n'} \rangle}$$

$$F_n S_{n' < n} = 0, \quad F_n S_n = K_n S_n$$

• Analogous deflation in continuous phase space:

$$\begin{split} F_n(\vec{r_0} \to \vec{r}) &= \\ &= \iiint dE d\hat{\Omega} dE_0 d\hat{\Omega}_0 \nu \Sigma_F(\vec{r}, E) \Big(G(\vec{r_0}, E_0, \hat{\Omega}_0 \to \vec{r}, E, \hat{\Omega}) - \sum_{n'=0}^{n-1} K_{n'} \frac{\Psi_{n'}(\vec{r}, E, \hat{\Omega}) \Psi_{n'}^{\dagger}(\vec{r_0}, E_0, \hat{\Omega}_0)}{\langle S_{n'}^{\dagger}(\vec{r'}) S_{n'}(\vec{r'}) \rangle} \Big) \frac{\chi(\vec{r_0}, E_0)}{4\pi} \end{split}$$

Supposition...

- Mode-0 adjoint weighting looks at neutron population after iterative application of the regular kernel
- Can higher mode adjoint weighting be performed with iterative application of the deflated kernel?

Aside: Relationship Between Green's Function and Flux Modes



K-eigenvalue transport:
$$\mathbf{M} \cdot \Psi(\vec{r}, E, \hat{\Omega}) = \frac{1}{K} \frac{\chi(\vec{r}, E)}{4\pi} S(\vec{r})$$

Expand (approximation):

$$\Psi(\vec{r}, E, \hat{\Omega}) = \sum_{n=0}^{\infty} c_n \Psi_n(\vec{r}, E, \hat{\Omega}) \quad , \quad S(\vec{r}) = \sum_{n=0}^{\infty} s_n S_n(\vec{r})$$

Find coefficients using biorthogonality & transport eq.:

$$s_n = \frac{\langle \Psi_n^{\dagger}(\vec{r}, E, \hat{\Omega}), \frac{\chi(\vec{r}, E)}{4\pi} S(\vec{r}) \rangle}{\langle \Psi_n^{\dagger}(\vec{r}, E, \hat{\Omega}), \frac{\chi(\vec{r}, E)}{4\pi} S_n(\vec{r}) \rangle} \quad , \quad c_n = \frac{K_n}{K_0} s_n$$

Insert into flux expansion:

$$\Psi(\vec{r}, E, \hat{\Omega}) = \frac{1}{K_0} \sum_{n=0}^{\infty} K_n \frac{\langle \Psi_n^{\dagger}(\vec{r}, E, \hat{\Omega}), \frac{\chi(\vec{r}, E)}{4\pi} S(\vec{r}) \rangle}{\langle \Psi_n^{\dagger}(\vec{r}, E, \hat{\Omega}), \frac{\chi(\vec{r}, E)}{4\pi} S_n(\vec{r}) \rangle} \Psi_n(\vec{r}, E, \hat{\Omega})$$

Recall the integral transport eq:

$$\Psi(\vec{r}, E, \hat{\Omega}) = \frac{1}{K_0} \iiint d\vec{r_0} dE_0 d\hat{\Omega} \frac{\chi(\vec{r_0}, E_0)}{4\pi} S(\vec{r_0}) G(\vec{r_0}, E_0, \hat{\Omega}_0 \to \vec{r}, E, \hat{\Omega})$$

Indicates Green's function expansion:

$$G(\vec{r}_0, E_0, \hat{\Omega}_0 \to \vec{r}, E, \hat{\Omega}) = \sum_{n=0}^{\infty} K_n \frac{\Psi_n(\vec{r}, E, \hat{\Omega}) \Psi_n^{\dagger}(\vec{r}_0, E, \hat{\Omega})}{\langle S_n^{\dagger}(\vec{r}\,'), S_n(\vec{r}\,') \rangle}$$



- Normal deflation alters a matrix--our 'matrix' is the random walk
- Approximate deflated kernel by separating its application on a source into,
 - Normal random walk
 - Matrix multiplication of outer product —

$$F_n(\vec{r_0} \to \vec{r}) \cdot S^c(\vec{r_0}) = F_0(\vec{r_0} \to \vec{r}) S^c(\vec{r_0}) - \sum_{n'=0}^{n-1} K_{n'} \frac{\langle S_{n'}^{\dagger}(\vec{r_0}) S^c(\vec{r_0}) \rangle}{\langle S_{n'}^{\dagger}(\vec{r'}) S_{n'}(\vec{r'}) \rangle} S_{n'}(\vec{r})$$

n'=0

Deflated fission kernel applied to fission bank Standard transport

Normalized inner-products of adjoint source modes & fission bank



- Normal deflation alters a matrix--our 'matrix' is the random walk
- Approximate deflated kernel by separating its application on a source into,
 - Normal random walk
 - Matrix multiplication of outer product

$$F_n(\vec{r_0} \to \vec{r}) \cdot S^c(\vec{r_0}) = F_0(\vec{r_0} \to \vec{r}) S^c(\vec{r_0}) - \sum_{n'=0}^{n-1} K_{n'} \frac{\langle S_{n'}^{\dagger}(\vec{r_0}) S^c(\vec{r_0}) \rangle}{\langle S_{n'}^{\dagger}(\vec{r'}) S_{n'}(\vec{r'}) \rangle} S_{n'}(\vec{r})$$

Deflated fission kernel applied to fission bank

Standard transport

Normalized inner-products of adjoint source modes & fission bank

- To apply deflated fission kernel F_n to fission bank,
 - Precompute forward/adjoint fission sources & eigenvalues with fission matrix
 - Start problem again with adjoint weighting on; before each cycle...
 - Bin fission bank into same spatial mesh as eigenvectors
 - Compute *n*-1 inner products and save for after next cycle
 - Run cycle--perform normal transport on fission bank
 - Bin new fission bank and subtract scaled forward fission source modes
 - Duplicate/delete sites in fission bank to replicate new vector
 - Aside: A vector of weights could be used to represent all modes desired

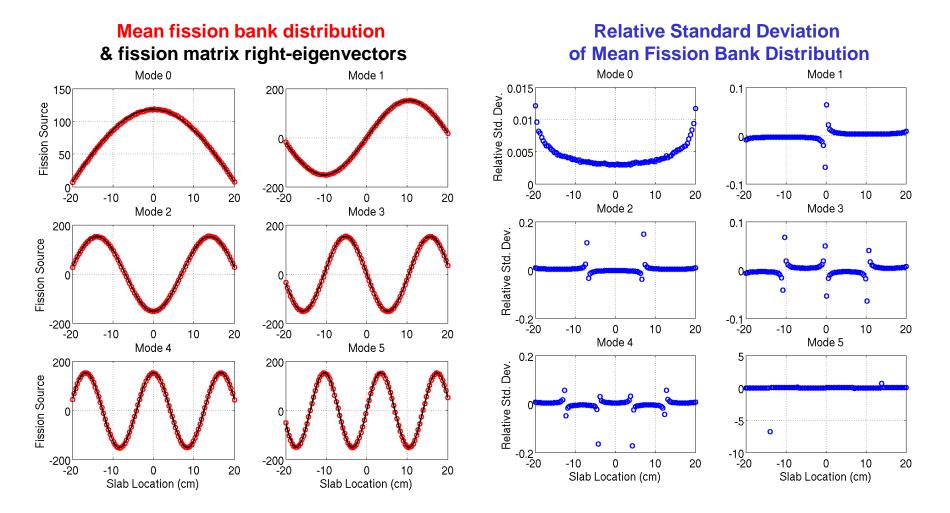


Tested kernel deflation with a 3-group (not self-adjoint), 40 cm slab problem Vacuum boundary conditions

g	Σ_t	Σ_f	Σ_{γ}	χ	$\Sigma_{s,g'1}$	$\Sigma_{s,g'2}$	$\Sigma_{s,g'3}$	$\bar{ u}$
1	0.7	0	0.05	1	0.45	0.2	0	0
2	1.2	0	0.05	0	0	0.55	0.6	0
3	1.2	0.05	0.05	0	0	0	1.1	2.17

- 1000 cycles ran, 10k batch size
 - initial guess: flat distribution

Ran 1000 cycles, 10k batch size, flat distribution as initial guess Statistics found from cycles 100-1000, wherein modes 0-5 were converged



Deflated fission banks stably oscillate about the true fission source mode

8-20-2013



Adjoint Flux Weighting



- Higher-mode adjoint weighting uses iterated fission probability, but with repeated application of deflated fission kernel
 - 0th mode—weigh tallies by fission rates of progeny in asymptotic generation
 - Higher modes—weigh by total population of progeny in asymptotic generation
- Verification--tally adjoint-weighted flux (compare with Matlab S_N code):

$$\int_{\vec{r}\in V_i} d\vec{r} \int_{E_g}^{E_{g-1}} dE \int_{4\pi} d\hat{\Omega} \ \Psi_n^{\dagger}(\vec{r}, E, \hat{\Omega}) \Psi_n(\vec{r}, E, \hat{\Omega})$$

- Positive/negative tally considerations:
 - Weighting factors in asymptotic generation are always positive
 - Flux tallies in original generation vary with sign
 - Absolute value of adjoint-weighted flux tallies at end-of-run are taken—assumes adjoint and forward flux are of same sign for given location in space
- Note: for perturbation & quasi-static calculations, want to compute:

$$\int_{\vec{r}} d\vec{r} \int_0^\infty dE \int_{4\pi} d\hat{\Omega} \ \Psi_n^{\dagger}(\vec{r}, E, \hat{\Omega}) \mathbf{A} \Psi_m(\vec{r}, E, \hat{\Omega}) \qquad \mathbf{A} \text{ is any operator}$$

0

5

10

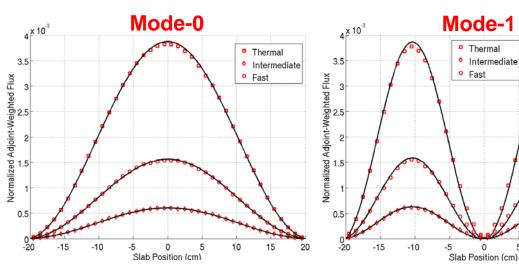
15

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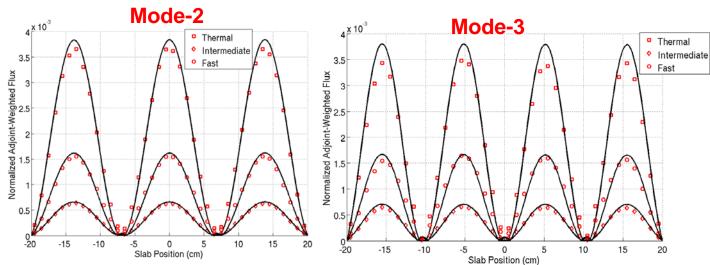


Ran 3015 cycles, 50k batch size, 20 latent generations Use relevant fission matrix source mode as initial guess Plot Monte Carlo & S₁₆ adjoint-weighted flux



$$\int_{\vec{r}\in V_i} d\vec{r} \int_{E_g}^{E_{g-1}} dE \int_{4\pi} d\hat{\Omega} \ \Psi_n^{\dagger}(\vec{r}, E, \hat{\Omega}) \Psi_n(\vec{r}, E, \hat{\Omega})$$

- **Increasing bias for higher** mode number (std. dev. is minor)
- **Overestimation near** inflection points
- Less analog treatment may be needed



Conclusions

- Fission matrix source modes can give insight into power iteration
- Running fixed source calculations on source modes give statisticallytractable tallies of forward flux modes
- Fission kernel deflation on a 3-group slab problem is stable, and gives correct estimates of forward source modes
- Higher-mode adjoint-weighting gives reasonable estimates for the 3-group slab problem

• Future Work

- Investigate bias seen in higher-mode adjoint-weighting, improve method
- Do higher-mode adjoint weighting on harder problems (asymmetric, multi-D, continuous energy)
- 2nd order perturbation theory & quasi-static methods
- Investigate sensitivity of higher source modes to meshing and statistics



Questions?