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Author(s):	Russell D. Mosteller
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## ENDF/B-V, ENDF/B-VI, AND ENDF/B-VII.0 RESULTS FOR THE DOPPLER-DEFECT BENCHMARK (u)

Russell D. Mosteller Los Alamos National Laboratory Los Alamos, NM 87545 mosteller@lanl.gov

#### ABSTRACT

A set of computational benchmarks for the Doppler reactivity defect has been specified for an infinite array of identical fuel pin cells containing normal or enriched UO<sub>2</sub> fuel, reactor-recycle mixed-oxide (MOX) fuel, or weapons-grade MOX fuel. The Doppler coefficient of reactivity, as well as the Doppler defect, can be computed for each of the cells. The MCNP5 Monte Carlo code was used to perform calculations for these benchmarks using cross sections derived from the ENDF/B-V, ENDF/B-VI, and ENDF/B-VII.0 nuclear data sets. The Doppler coefficients obtained from the three data sets exhibit very similar behavior. The Doppler coefficient for UO<sub>2</sub> fuel becomes less negative with increasing enrichment, with a generally asymptotic shape. The Doppler coefficient for the reactor-recycle MOX becomes less negative with increasing PuO<sub>2</sub> content but exhibits less curvature than that for UO<sub>2</sub> fuel. The Doppler coefficient for weapons-grade MOX shows a pronounced shoulder btween 1 wt.% and 2 wt.% PuO<sub>2</sub>, with a nearly constant value thereafter. The Doppler coefficient for heavily loaded MOX fuel, whether reactor-recycle or weapons-grade, is significantly more negative than that for highly enriched UO<sub>2</sub> fuel.

Key Words: Doppler, Benchmark, ENDF/B-V, ENDF/B-VI, ENDF/B-VII.0, UO2, MOX

#### 1. INTRODUCTION

A set of computational benchmarks [1] for the Doppler reactivity defect has been specified for an infinite array of identical fuel pin cells containing normal or enriched UO<sub>2</sub> fuel, reactorrecycle mixed-oxide (MOX) fuel, or weapons-grade MOX fuel. There are corresponding pairs of pin cells for hot-zero-power (HZP) and hot-full-power (HFP) conditions. At HZP everything – fuel, cladding, and borated moderator – is at a uniform 600 K. At HFP, the fuel is at 900 K, while everything else still is at 600 K. The soluble boron concentration in the moderator is 1400 ppm for all cases. The Doppler defect can be calculated as the reactivity difference between HFP and HZP conditions, and the Doppler coefficient is simply the Doppler defect divided by the change in the fuel temperature. Specifically,

$$DC = \frac{\Delta \rho_{Dop}}{\Delta T_{Fuel}}$$

where DC is the Doppler coefficient of reactivity,  $\Delta T_{Fuel}$  is 300 K, and the Doppler defect is

$$\Delta \rho_{Dop} = \frac{k_{HFP} - k_{HZP}}{k_{HFP} * k_{HZP}}$$

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There are three subsets of benchmarks, but the pin cells for all three are identical except for the fuel they contain. The first subset contains  $UO_2$  fuel, ranging from normal to 5.0 wt.% enriched uranium. The second subset contains reactor-recycle MOX, with 1 wt.% to 8 wt.%  $PuO_2$ . The third subset contains weapons-grade MOX, with 1 wt.% to 6 wt.%  $PuO_2$ . The plutonium isotopics for the two types of MOX cases are summarized in Table I.

Fuel	<sup>239</sup> Pu	<sup>240</sup> Pu	<sup>241</sup> Pu	<sup>242</sup> Pu
Reactor-Recycle MOX	45.0	30.0	15.0	10.0
Weapons-Grade MOX	93.6	5.9	0.4	0.1

Table I. Plutonium Isotopics (at.%)

## 2. CALCULATIONS

The calculations were performed with the MCNP5 Monte Carlo code [2], using cross sections based on ENDF/B-V [3], ENDF/B-VI [4], and ENDF/B-VII.0 [5]. The basic nuclear data for all three cross-section sets had been generated previously from the corresponding ENDF/B data files with the NJOY code [6]. However, many of the cross sections needed for the ENDF/B-VI and ENDF/B-VII.0 calculations were not readily available at 600 K and/or 900 K. Accordingly, the DOPPLER code [7,8] was employed to generate cross sections at those temperatures from the cross sections that were available.

The ENDF/B-V nuclear data were generated many years ago for two sets of benchmarks [9,10,11] that have been altered slightly and then subsumed into the current set. The basic ENDF/B-VI cross sections were taken from the ENDF66 [12] and ACTI [13] libraries that were included in the MCNP5 distribution. That combination of cross sections corresponds to the final release of ENDF/B-VI. The basic ENDF/B-VII.0 cross sections were processed directly from the initial release that occurred in December 2006.

Each MCNP5 calculation employed 550 generations of 10,000 neutrons each. The first 50 generations were excluded from the statistics. Consequently, the values of  $k_{eff}$  obtained from these calculations each are based on 5,000,000 active neutron histories. This number of histories is considered sufficient because it reduces the uncertainty in the Doppler coefficient to 5% or less for all cases. In practical applications, uncertainties as high as 10% in the Doppler coefficients have been considered acceptable.

## 3. RESULTS

The value obtained for  $k_{eff}$  and for the Doppler coefficients for for the UO<sub>2</sub> cases are presented in Table II, and the resulting Doppler coefficients are plotted in Figure 1. ENDF/B-V and ENDF/B-VI produce very similar values for  $k_{eff}$ , with the difference between corresponding results usually less than 10 pcm. ENDF/B-VII.0 produces higher values for  $k_{eff}$  than either

ENDF/B-V or ENDF/B-VI for every case. However, all three nuclear data sets produce very similar results for the Doppler coefficients. In fact, the Doppler coefficients from the three libraries are within a single standard deviation of each other at each enrichment except 5 wt.%. The Doppler coefficient becomes less negative with increasing enrichment, and the curve appears to take on an asymptotic shape.

Nuclear	P 11	k	Doppler	
Library	(wt.%)	HFP	HZP	(pcm/K)
ENDF/B-V	0.711 1.6 2.4 3.1 3.9 4.5 5.0	$\begin{array}{c} 0.65946 \pm 0.00019 \\ 0.95155 \pm 0.00026 \\ 1.08900 \pm 0.00027 \\ 1.16636 \pm 0.00027 \\ 1.22875 \pm 0.00028 \\ 1.26448 \pm 0.00028 \\ 1.28888 \pm 0.00029 \end{array}$	$\begin{array}{c} 0.66481 \pm 0.00019 \\ 0.95928 \pm 0.00026 \\ 1.09750 \pm 0.00026 \\ 1.17563 \pm 0.00028 \\ 1.23877 \pm 0.00029 \\ 1.27451 \pm 0.00030 \\ 1.29885 \pm 0.00030 \end{array}$	$\begin{array}{c} -4.07 \pm 0.20 \\ -2.82 \pm 0.13 \\ -2.37 \pm 0.10 \\ -2.25 \pm 0.09 \\ -2.19 \pm 0.09 \\ -2.07 \pm 0.08 \\ -1.99 \pm 0.08 \end{array}$
ENDF/B-VI	0.711 1.6 2.4 3.1 3.9 4.5 5.0	$\begin{array}{c} 0.65953 \pm 0.00019 \\ 0.95107 \pm 0.00025 \\ 1.08774 \pm 0.00028 \\ 1.16542 \pm 0.00027 \\ 1.22765 \pm 0.00030 \\ 1.26240 \pm 0.00027 \\ 1.28669 \pm 0.00030 \end{array}$	$\begin{array}{c} 0.66500 \pm 0.00020\\ 0.95906 \pm 0.00025\\ 1.09638 \pm 0.00027\\ 1.17485 \pm 0.00029\\ 1.23733 \pm 0.00027\\ 1.27264 \pm 0.00028\\ 1.29690 \pm 0.00030\\ \end{array}$	$\begin{array}{c} -4.16 \pm 0.21 \\ -2.92 \pm 0.13 \\ -2.41 \pm 0.11 \\ -2.30 \pm 0.10 \\ -2.12 \pm 0.09 \\ -2.12 \pm 0.08 \\ -2.04 \pm 0.08 \end{array}$
ENDF/B-VII.0	0.711 1.6 2.4 3.1 3.9 4.5 5.0	$\begin{array}{c} 0.66108 \pm 0.00018\\ 0.95411 \pm 0.00026\\ 1.09077 \pm 0.00028\\ 1.16794 \pm 0.00028\\ 1.23048 \pm 0.00029\\ 1.26598 \pm 0.00029\\ 1.28959 \pm 0.00031 \end{array}$	$\begin{array}{c} 0.66661 \pm 0.00019 \\ 0.96176 \pm 0.00027 \\ 1.09955 \pm 0.00027 \\ 1.17741 \pm 0.00029 \\ 1.24054 \pm 0.00032 \\ 1.27621 \pm 0.00028 \\ 1.30027 \pm 0.00029 \end{array}$	$\begin{array}{c} -4.18 \pm 0.20 \\ -2.78 \pm 0.14 \\ -2.44 \pm 0.11 \\ -2.30 \pm 0.10 \\ -2.20 \pm 0.09 \\ -2.11 \pm 0.08 \\ -2.12 \pm 0.08 \end{array}$

Table II. Results for UO<sub>2</sub> Pin Cells

The values obtained for  $k_{eff}$  and for the Doppler coefficients for the reactor-recycle MOX cases are given in Table III, and the resulting Doppler coefficients are plotted in Figure 2. The ENDF/B-V values for  $k_{eff}$  increase more slowly with plutonium content than do the corresponding values from ENDF/B-VI or ENDF/B-VII.0. In contrast, the ENDF/B-VI and ENDF/B-VII.0 values are quite consistent with each other. Once again, however, all three data sets produce very similar results for the Doppler coefficients. In fact, the three results for the Doppler coefficient are within a single standard deviation of each other at each of the PuO<sub>2</sub> concentrations. The curves for the Doppler coefficients are nearly linear but slightly convex.

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Figure 1. Doppler Coefficient for Normal and Enriched UO2 Fuel

The values obtained for k<sub>eff</sub> and for the Doppler coefficients obtained for the weapons-grade MOX cases are shown in Table IV, and the Doppler coefficients are plotted in Figure 3. The ENDF/B-V values for k<sub>eff</sub> increase more slowly with plutonium content than do the corresponding values from ENDF/B-VI or ENDF/B-VII.0. However, in contrast with the reactor-recycle results, the ENDF/B-VI values for k<sub>eff</sub> are consistently lower than those from ENDF/B-VI values. Nonetheless, all three nuclear data sets once again produce very similar results for the Doppler coefficient. In fact, the Doppler coefficients from the three nuclear data libraries are within a single standard deviation for all but one of the PuO<sub>2</sub> concentrations (4.0 wt.%). In contrast to the behavior exhibited by the Doppler coefficients for UO<sub>2</sub> and reactor-recycle MOX fuel, the Doppler coefficient for the weapons-grade MOX has a pronounced shoulder at a PuO<sub>2</sub> content between 1 wt.% and 2 wt.%. Thereafter, ENDF/B-V produces a curve that is nearly flat, while both ENDF/B-VI and ENDF/B-VII.0 produce curves that become slightly less negative with increasing PuO<sub>2</sub> content.

It is worth noting that the Doppler coefficients for both reactor-recycle and weapons-grade MOX fuel show considerably less variation with  $PuO_2$  content than the Doppler coefficient for  $UO_2$  fuel shows with enrichment. Furthermore, for practical loadings, the Doppler coefficient for high MOX loadings is significantly more negative than the Doppler coefficient for highly enriched  $UO_2$  fuel.

Nuclear	MOX Content (wt.%)	k	Doppler	
Data Library		HFP	HZP	(pcm/K)
ENDF/B-V	1.0 2.0 4.0 6.0 8.0	$\begin{array}{c} 0.93331 \pm 0.00026 \\ 1.00745 \pm 0.00029 \\ 1.06157 \pm 0.00030 \\ 1.08988 \pm 0.00031 \\ 1.11314 \pm 0.00031 \end{array}$	$\begin{array}{c} 0.94342 \pm 0.00026 \\ 1.01884 \pm 0.00030 \\ 1.07329 \pm 0.00029 \\ 1.10180 \pm 0.00032 \\ 1.12534 \pm 0.00030 \end{array}$	$\begin{array}{c} -3.83 \pm 0.14 \\ -3.70 \pm 0.14 \\ -3.43 \pm 0.12 \\ -3.31 \pm 0.12 \\ -3.25 \pm 0.11 \end{array}$
ENDF/B-VI	1.0 2.0 4.0 6.0 8.0	$\begin{array}{c} 0.93303 \pm 0.00027 \\ 1.00839 \pm 0.00030 \\ 1.06440 \pm 0.00031 \\ 1.09309 \pm 0.00032 \\ 1.11694 \pm 0.00031 \end{array}$	$\begin{array}{c} 0.94334 \pm 0.00029 \\ 1.02015 \pm 0.00030 \\ 1.07638 \pm 0.00031 \\ 1.10532 \pm 0.00032 \\ 1.12915 \pm 0.00030 \end{array}$	$-3.90 \pm 0.15$ $-3.76 \pm 0.14$ $-3.49 \pm 0.13$ $-3.37 \pm 0.12$ $-3.23 \pm 0.12$
ENDF/B-VII.0	1.0 2.0 4.0 6.0 8.0	$\begin{array}{c} 0.93451 \pm 0.00027 \\ 1.00974 \pm 0.00029 \\ 1.06468 \pm 0.00033 \\ 1.09385 \pm 0.00032 \\ 1.11694 \pm 0.00032 \end{array}$	$\begin{array}{c} 0.94448 \pm 0.00028 \\ 1.02106 \pm 0.00032 \\ 1.07643 \pm 0.00032 \\ 1.10568 \pm 0.00032 \\ 1.12880 \pm 0.00031 \end{array}$	$-3.77 \pm 0.15$ $-3.66 \pm 0.14$ $-3.42 \pm 0.13$ $-3.26 \pm 0.12$ $-3.14 \pm 0.12$

Table III. Results for Reactor-Recycle MOX Pin Cells



Figure 2. Doppler Coefficient for Reactor-Recycle MOX Fuel

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Nuclear	MOX Content (wt.%)	k	Doppler	
Library		HFP	HZP	(pcm/K)
ENDF/B-V	1.0 2.0 4.0 6.0	$\begin{array}{c} 1.07945 \pm 0.00029 \\ 1.16785 \pm 0.00029 \\ 1.23410 \pm 0.00029 \\ 1.26905 \pm 0.00029 \end{array}$	$\begin{array}{c} 1.08911 \pm 0.00026 \\ 1.17847 \pm 0.00028 \\ 1.24574 \pm 0.00029 \\ 1.28160 \pm 0.00029 \end{array}$	$\begin{array}{c} -2.74 \pm 0.11 \\ -2.57 \pm 0.10 \\ -2.52 \pm 0.09 \\ -2.57 \pm 0.08 \end{array}$
ENDF/B-VI	1.0 2.0 4.0 6.0	$\begin{array}{c} 1.07812 \pm 0.00027 \\ 1.16813 \pm 0.00028 \\ 1.23620 \pm 0.00029 \\ 1.27284 \pm 0.00030 \end{array}$	$\begin{array}{c} 1.08821 \pm 0.00027 \\ 1.17920 \pm 0.00029 \\ 1.24839 \pm 0.00030 \\ 1.28493 \pm 0.00031 \end{array}$	$-2.87 \pm 0.11$ $-2.68 \pm 0.10$ $-2.63 \pm 0.09$ $-2.46 \pm 0.09$
ENDF/B-VII.0	1.0 2.0 4.0 6.0	$\begin{array}{c} 1.08002 \pm 0.00027 \\ 1.17055 \pm 0.00029 \\ 1.23823 \pm 0.00030 \\ 1.27495 \pm 0.00030 \end{array}$	$\begin{array}{c} 1.09000 \pm 0.00027 \\ 1.18180 \pm 0.00029 \\ 1.25067 \pm 0.00029 \\ 1.28722 \pm 0.00031 \end{array}$	$-2.83 \pm 0.11$ $-2.71 \pm 0.10$ $-2.68 \pm 0.09$ $-2.49 \pm 0.09$

Table IV. Results for Weapons-Grade MOX Pin Cells



Figure 3. Doppler Coefficient for Weapons-Grade MOX Fuel

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## 4. SUMMARY AND CONCLUSIONS

Calculations with cross sections derived from ENDF/B-V, ENDF/B-VI, and ENDF/B-VII.0 have been performed for all of the cases in the benchmark specifications for the Doppler defect. All three data sets produce very similar results, so similar in fact that for nearly all of the cases the Doppler coefficients from the three nuclear data libraries are statistically indistinguishable. Consequently, even though differences can be observed in the values for  $k_{eff}$ , in practical terms it doesn't much matter which of the three nuclear data libraries is used to calculate the Doppler coefficient.

The behavior of the Doppler coefficients for the UO2, reactor-recycle MOX, and weapons-grade MOX are significantly different, however. The Doppler coefficient for  $UO_2$  fuel follows an approximately asymptotic curve that becomes less negative with increasing enrichment. The Doppler coefficients for the reactor-recycle MOX cases produce a nearly linear curve that is only slightly convex as a function of increasing plutonium content. The Doppler coefficients for the weapons-grade MOX cases produce a fairly sharp shoulder, after which the coefficient more slowly becomes less negative or remains essentially constant.

In addition, it should be noted that the Doppler coefficient for heavy loadings of MOX fuel is significantly more negative than the Doppler coefficient for highly enriched UO<sub>2</sub> fuel.

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